

## Tuning and Analysis of Fractional Order PID Controller

Vineet Shekher<sup>1</sup>, Pankaj Rai<sup>2</sup> and Om Prakash<sup>3</sup>

<sup>1</sup>Assistant Professor, Hindu College of Engineering, Sonapat, Haryana, India

<sup>2</sup>Head, Electrical Engineering, Birsa Institute of Technology,  
Sindri, Dhanbad, Jharkhand, India

<sup>3</sup>Associate Professor, Chemical Engineering,  
Birsa Institute of Technology, Sindri, Dhanbad, Jharkhand India

### Abstract

This paper presents the development of a new tuning method and performance of the fractional order PID controller includes the integer order PID controller parameter. The tuning of the PID controller is mostly done using Zeigler and Nichols tuning method. All the parameters of the controller, namely  $K_p$  (Proportional gain),  $K_i$  (integral gain),  $K_d$  (derivative gain) can be determined by using Zeigler and Nichols method. Fractional order PID (FOPID) is a special kind of PID controller whose derivative and integral order are fractional rather than integer. To design FOPID controller is to determine the two important parameters  $\lambda$  (integrator order) and  $\mu$  (derivative order). In this paper it is shown that the response and performance of FOPID controller is much better than integer order PID controller for the same system.

### Introduction

PID controller is a well known controller which is used in the most application. PID controller becomes a most popular industrial controller due to its simplicity and the ability to tune a few parameters automatically. According to the Japan electric measuring instrument manufacture's association in 1989, PID controller is used in more than 90% of the control loop. As an example for the application of PID controller in industry, slow industrial process can be pointed, low percentage overshoot and small settling time can be obtained by using this controller. This controller provides feedback, it has ability to eliminate steady state offsets through derivative action. The derivative action in the control loop will improve the damping and therefore by accelerating the transient response, a lighter proportional gain can be

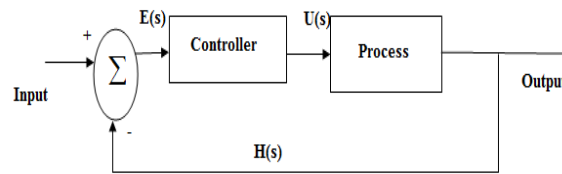
obtained during the past half century, many theoretical and industrial studies have been done in PID controller setting rules Zeigler and Nichol's in 1942 proposed a method to set the PID controller parameter Hagglund and Astrom in 1955 and cheng-ching in 1999, introduced other technique. By generalizing the derivative and integer orders, from the integer field to non-integer numbers, the fractional order PID control is obtained.

The performance of the PID controller can be improved by making the use of fractional order derivatives and integrals. This flexibility helps the design more robust system. Before using the fractional order controller in design an introduction to the fractional calculus is required. The first time, calculus generation to fractional, was proposed Leibniz and Hopital for the first time afterwards, the systematic studies in this field by many researchers such as Liouville (1832), Holmgren (1864) and Riemann (1953) were performed.

### Integer Order PID Controller

The PID refers to the first letter of the names that make up the standard three term controller. These are P for the proportional term, I for the Integral term and D for the derivative term in the controller. Three term or PID controllers are probably used by most widely industrial controller.

A PID controller is essentially a generic closed loop feedback mechanism.



**Figure 1:** SISO unity feedback controller

Controller monitors the error between a measured process variable and a desired set point; from this error, a corrective signal is computed and is eventually feedback to the input side to adjust the process accordingly. The differential equation for the PID controller is

$$u(t) = K_p e(t) + T_i \int_0^t e_p(t) dt + T_d \frac{d}{dt} e(t) dt \quad (1)$$

Thus, the PID controller algorithm is described by a weighted sum of the three time functions where the three distinct weights are:  $K_p$  (Proportional gain) determines the influence of the present error value on the control mechanism, I (integral gain) decides the reaction based on the area under the error time curve up to

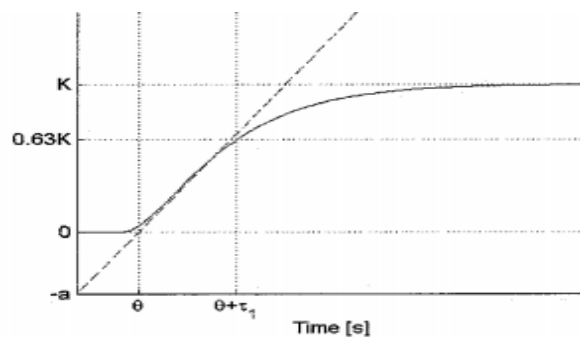
the present point and  $T_d$  (derivative gain) accounts for the extent of the reaction to the rate of change of the error with time.

**Tuning of Integer Order PID Controller**

Many tuning method are presented in literature that are based on a few structure of the process dynamics.

**Zeigler Nichols Process Reaction Curve Method**

In 1942, Zeigler and Nichols presented two classical methods to tune a PID controller. These methods are widely used, due to their simplicity. In the first method, the controller setting are based on two parameter  $\theta$  and  $a$  of the process reaction curve.



The proposed Zeigler Nichols setting is shown Table 1

Controller Type	$K_p$	$T_i$	$T_d$
P	$1/a$	-----	-----
PI	$0.9/a$	$3.33a$	-----
PID	$1.2/a$	$2\theta$	$0.5\theta$

The frequency domain method proposed by Zeigler and Nichols is based on the ultimate gain  $K_c$  and the ultimate period  $T_u$ . The controller setting is shown Table 2

Controller Type	$K_p$	$T_i$	$T_d$
P	$0.5K_c$	-----	-----
PI	$0.45K_c$	$0.83T_u$	-----
PID	$0.6K_c$	$0.5T_u$	$0.125T_u$

### Astrom and Haggland (1985)

Astrom and Haggland recognized that the Zeigler-Nichols continuous cycling method actually identifies the point  $(-1/K_u, 0)$  on the Nyquist curve, and move it to a predefined point. With PID control, it is possible to move a given point on the Nyquist curve to an arbitrary position. By increasing the gain, the arbitrary point moves in the direction of  $G(j\omega)$ . By changing I and D action moves the point in the orthogonal direction.

### Brief Mathematical Background of Fractional calculus

Orders of fractional calculus are real number. Many different definitions for general integro- differential operation can be found in the literature. Among them the most commonly used for general fractional Integro- differential expressions are given by chauchy, Riemann-Liouville, Grunwald letnikov and Caputo. These definitions are required for realization of control algorithm.

At first, we generalize the differential and Integral operators in to one fundamental operator  ${}_a D_t^\alpha$  where

$$\begin{aligned} {}_a D_t^\alpha &= \frac{d^\alpha}{dt^\alpha} \text{ for } R(\alpha) > 0 \\ &= 1 \text{ for } R(\alpha) = 0 \\ &= \int_a^t (d\tau)^{-\alpha} \text{ for } R(\alpha) < 0 \end{aligned}$$

$R(\alpha)$  Denote real part of the  $\alpha$  which is, in general is a complex quantity.

The Grunwald – Letnikov definition is

$${}_a D_t^\alpha f(t) = \lim_{h \rightarrow 0} \frac{1}{h^\alpha} \sum_{j=0}^{\lceil \frac{t-a}{h} \rceil} (-1)^j \binom{\alpha}{j} f(t - jh)$$

The fractional order for the first order system is given by in the figure (1)

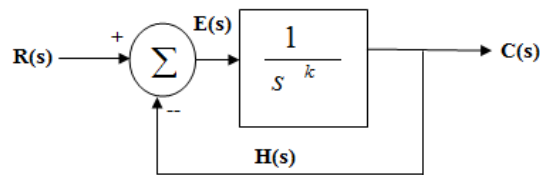


Figure 2

The transfer function is given by

$$\frac{C(s)}{R(s)} = \frac{1}{s^k + 1} \quad (2)$$

By putting  $s = j\omega$ , the closed loop transfer function given by  $H(j\omega)$

$$\begin{aligned}
 H(j\omega) &= \frac{1}{(j\omega)^k + 1}; \text{ where } j^k = \cos\frac{\pi K}{2} + j\sin\frac{\pi K}{2} \\
 H(j\omega) &= \frac{1}{\omega^k (\cos\frac{\pi K}{2} + j\sin\frac{\pi K}{2}) + 1} \\
 H(j\omega) &= \frac{1}{(\omega^k \cos\frac{\pi K}{2} + 1) + j\sin\frac{\pi K}{2} \omega^k} \tag{3}
 \end{aligned}$$

For the system design, we need the maximum value of  $|H(j\omega)|$  and frequency  $\omega_p$  where the maximum occur where

$$\begin{aligned}
 |H(j\omega)| &= \frac{1}{\sqrt{\omega^{2k} + 1 + 2\omega^k \cos\frac{\pi K}{2}}} \text{ and} \\
 \text{Arg } H(j\omega) &= -\tan^{-1}\left(\frac{\omega^k \sin\frac{\pi K}{2}}{1 + \omega^k \cos\frac{\pi K}{2}}\right) \tag{4}
 \end{aligned}$$

A fractional differential equation for a fractional order control system can be written as

$$\begin{aligned}
 a_n \frac{d^{\alpha_n} y(t)}{dt^{\alpha_n}} + a_{n-1} \frac{d^{\alpha_{n-1}} y(t)}{dt^{\alpha_{n-1}}} + \dots + a_0 \frac{d^{\alpha_0} y(t)}{dt^{\alpha_0}} \\
 = b_m \frac{d^{\beta_m} x(t)}{dt^{\beta_m}} + b_{m-1} \frac{d^{\beta_{m-1}} x(t)}{dt^{\beta_{m-1}}} + \dots + b_0 \frac{d^{\beta_0} x(t)}{dt^{\beta_0}}
 \end{aligned}$$

Where  $\alpha_n > \alpha_{n-1} > \dots > \alpha_0 \geq 0$  and  $\beta_n > \beta_{n-1} > \dots > \beta_0 \geq 0$  are constant.

**Basic concept of Fractional order PID controller**

Consider the negative feedback control system as shown in fig (2).

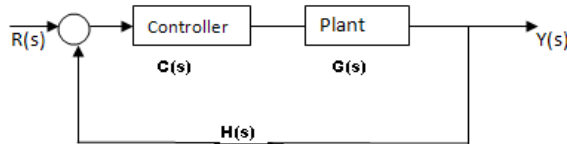


Figure 2

The continuous transfer function of the  $PI^\lambda D^\mu$  controller is obtained through Laplace transform as

$$C(s) = K_p + \frac{T_i}{s^\lambda} + T_d s^\mu \quad (5)$$

The PID controller expands the integer order PID controller from point to plane, there by adding flexibility to controller design and allowing us to control our real world processes more accurately but only at the cost of increased design complexity.

### Tuning method for the fraction order PID controller

To obtain the  $K_p$  (proportional gain), a constant of integral term ( $K_i$ ), the constant of derivative term  $K_d$ , the fractional order of differentiator  $\mu$  and the fractional order of integrator  $\lambda$ . The method uses classical Zeigler – Nichols tuning rule to obtain  $K_p$  and  $K_i$ . To obtain initial value of  $K_d$ , then some fine tuning has been done by using Astrom-Hagglund method described earlier. The fractional order  $\lambda$  and  $\mu$  are obtained to achieve specified phase margin.

Let  $\phi_{pm}$  be the required phase margin and  $\omega_{cp}$  be the frequency of the critical point on the Nyquist curve of  $G(s)$  at which  $\arg(G(j\omega_{cp})) = -180^\circ$ , then the gain margin defined as

$$g_m = \frac{1}{|G(j\omega_{cp})|} = K_c \quad (6)$$

In order to make the phase margin of the system equal to  $\phi_{pm}$  and  $|C(j\omega_{cp})G(j\omega_{cp})| = 1$ , the following equation must be satisfied.

$$C(j\omega_{cp}) = \frac{1}{|G(j\omega_{cp})|} e^{j\phi_{pm}} = K_c \cos \phi_{pm} + jK_c \sin \phi_{pm} \quad (7)$$

Then we write  $C(j\omega_{cp})$  using equation

$$C(j\omega_{cp}) = K_p + K_i \omega_{cp}^{-\lambda} \cos\left(\frac{\pi}{2}\lambda\right) + K_d \omega_{cp}^\mu \cos\left(\frac{\pi}{2}\mu\right) + \left[ -K_i \omega_{cp}^{-\lambda} \sin\left(\frac{\pi}{2}\lambda\right) + K_d \omega_{cp}^\mu \sin\left(\frac{\pi}{2}\mu\right) \right] \quad (8)$$

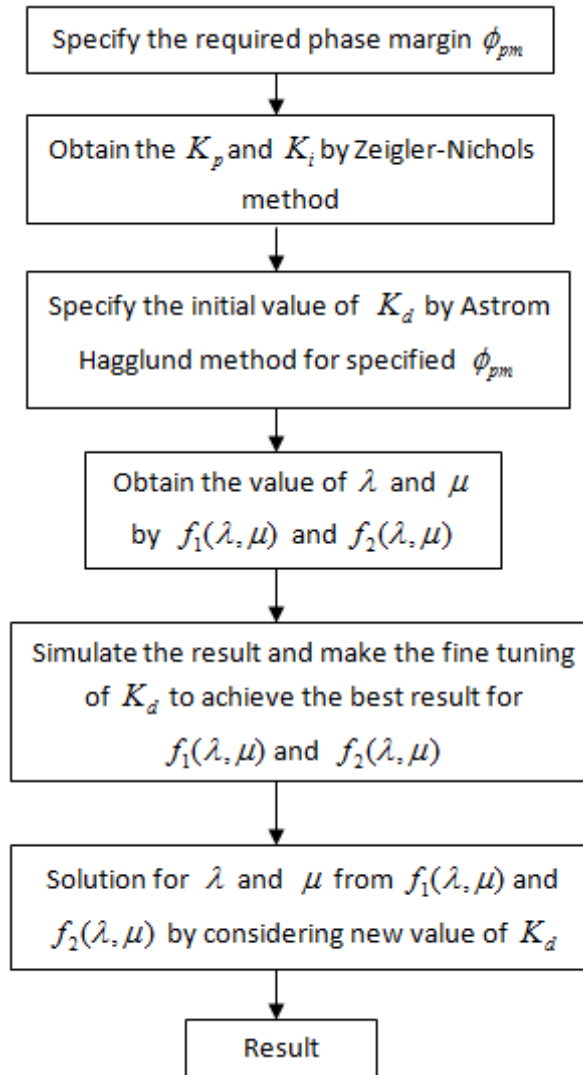
Considering equation (7) and (8) we can write

$$f_1(\lambda, \mu) = K_p + K_i \omega_{cp}^{-\lambda} \cos\left(\frac{\pi}{2}\lambda\right) + K_d \omega_{cp}^\mu \cos\left(\frac{\pi}{2}\mu\right) - K_c \cos \phi_{pm} = 0 \quad (9)$$

$$f_2(\lambda, \mu) = -K_i \omega_{cp}^{-\lambda} \sin\left(\frac{\pi}{2}\lambda\right) + K_d \omega_{cp}^\mu \sin\left(\frac{\pi}{2}\mu\right) - K_c \sin \phi_{pm} = 0 \quad (10)$$

The numerical solution for  $\lambda$  and  $\mu$  can be obtained by the equation (9) and (10).

### Algorithm for tuning of $PI^\lambda D^\mu$ controller



### Problem formulation

The transfer function consider for the implementation of PID and FOPID controller is given as

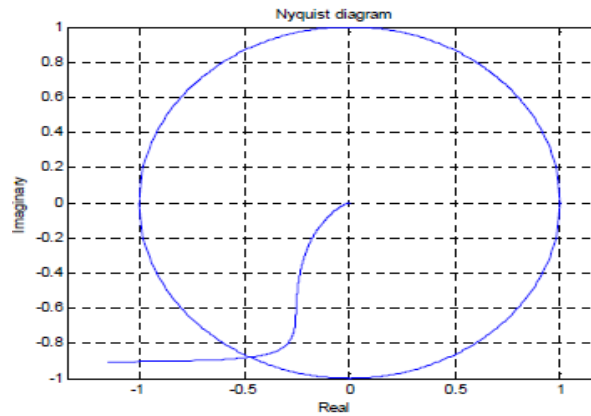
$$G(s) = \frac{1}{s(s^2 + 3s + 2)}$$

By using Routh's stability, the phase crossover frequency of the system can be defined as  $\omega_{cp} = \sqrt{2}$  and the gain margin of the system can be obtained as  $K_c = 6$ .

To tune the PID controller, Zeigler Nichols closed loop tuning is used.  $K_p, K_i$  and  $K_d$  of the controller has been obtained are 3.6, 1.63 and 1.98. The PID controller obtain can be given as  $C_1(s)$

$$C_1(s) = 3.6 + \frac{1.63}{s} + 1.98s$$

By using classical Astrom Hagglund method, the value of the PID controller parameters have been calculated for the specified phase margin ( $\phi_{pm}$ ) at  $40^\circ$ .



**Figure 3**

**Table 3**

Parameter	Z-N Method value	Phase Angle	Astrom method value
$K_p$	3.6	$40^\circ$	4.59
$K_i$	1.63	$40^\circ$	1.51
$K_d$	1.98	$40^\circ$	3.48

The controller obtained by classical Astrom Hagglund method is given by

$$C_2(s) = 4.59 + \frac{1.51}{s} + 3.48s$$

The proposed method takes the value of  $K_p$  and  $K_i$  from Zeigler and Nichols method. The value of  $K_d$  have been obtained by using Astrom - Hagglund method for



specified Phase Margin ( $\phi_{pm} = 40^0$ ). By using fine tuning for  $K_d$  to achieve the best solution by equation (9) and (10) for the specified phase margin.

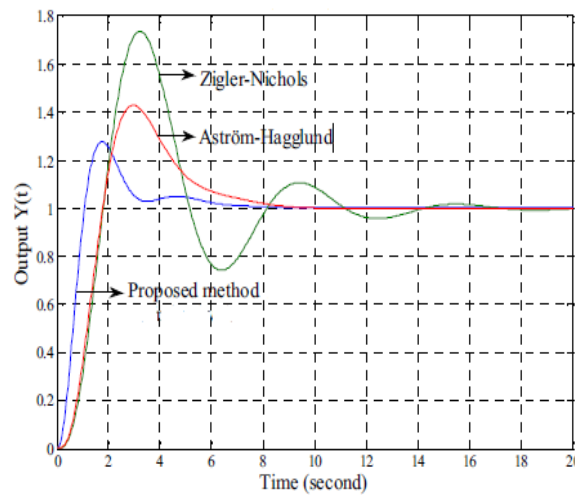
These two equations can be solved by using “fsolve” toolbox of the MATLAB to obtain the value of  $\lambda$  and  $\mu$  for the new value of  $K_d$  for the phase margin ( $\phi_{pm} = 40^0$ ).

Phase Margin	Proposed Method				
	$K_p$	$K_i$	$K_d$	$\lambda$	$\mu$
$40^0$	3.6	1.63	3.75	1.39	0.79

The  $PI^\lambda D^\mu$  controller obtained can be written as

$$C_3(s) = 3.6 + \frac{1.63}{s^{1.39}} + 3.75s^{0.79}$$

Step response of the system for  $C_1(s)$ ,  $C_2(s)$  and  $C_3(s)$  for  $40^0$  phase margin are given in figure (3).



**Figure 3**

Step response of the system gives valuable information such as Maximum overshoot ( $M_p\%$ ), rise time ( $T_r$ ), peak time ( $T_p$ ) and settling time ( $T_s$ ).

Step Response specification	Maximum Overshoot $M_p\%$	Peak time $T_r$	Rise Time $T_p$	Settling time $T_s$
Z-N PID	73.5	3.25	1.67	12.5
A-H PID	43.0	2.95	1.66	6.67
FO-PID	27.9	1.74	0.96	4.65

From the table the proposed method gives much better performance with respect to Z-N method and Astrom-Hagglund method especially for Maximum overshoot ( $M_p\%$ ), rise time( $T_r$ ), peak time( $T_p$ ) and settling time( $T_s$ ).

## Conclusion

A method for tuning of PID and fractional order PID controller has been proposed. The presented method is based on idea of using Zeigler-Nichols for  $K_p$  and  $K_i$  while Astrom-Hagglund method is used for determining  $K_d$  for the conventional PID. Similarly  $K_p$  and  $K_i$  parameter for fractional order PID controller have been computed from Zeigler and Nichols method and the remaining parameter  $K_d$ ,  $\lambda$  and  $\mu$  have been found from Astrom - Hagglund method. The simulation result demonstrated that the fractional order PID controller has better response than the conventional PID controller. The comparison study of the proposed method for tuning of fractional order PID controller certainly will be very important. FOPID controller provides stability region even when an Integer order PID controller cannot provide any stability region.

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